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IS 3588 (1987): Electric Axial Flow Fans [ETD 5: Electric Fans]



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*Indian Standard*

**SPECIFICATION FOR  
ELECTRIC AXIAL FLOW FANS**

*( First Revision )*

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**BUREAU OF INDIAN STANDARDS**  
MANAK BHAVAN, 9 BAHADUR SHAH ZAFAR MARG  
NEW DELHI 110002

# Indian Standard

## SPECIFICATION FOR ELECTRIC AXIAL FLOW FANS

### ( First Revision )

#### 0. FOREWORD

**0.1** This Indian Standard ( First Revision ) was adopted by the Bureau of Indian Standards on 27 August 1987, after the draft finalized by the Electric Fans Sectional Committee had been approved by the Electrotechnical Division Council.

**0.2** The axial flow fans covered by this standard are capable of working against pressures and are distinct from the table, ceiling or pedestal type fans which also are considered to be axial flow fans. The main difference between these two is that latter category works under free flow conditions and the pressure developed is very low, of the order of 0.5 mmH<sub>2</sub>O.

**0.3** This standard was originally published in 1966. The present revision has been undertaken to take into account the experience gained since then and to align some of the safety requirements

with the provisions of IS : 302-1979\*. The amendments issued to the previous edition of the standard have also been incorporated, to the extent applicable.

**0.4** In preparing this standard, some assistance has been drawn from BS 848 : Part 1 : 1980 'Fans for general purposes : Part 1 Methods of testing performance', issued by the British Standards Institution.

**0.5** For the purpose of deciding whether a particular requirement of this standard is complied with, the final value, observed or calculated, expressing the result of a test, shall be rounded off in accordance with IS : 2-1960†. The number of significant places retained in the rounded off value should be the same as that of the specified value in this standard.

\*General and safety requirements for household and similar electrical appliances (*fifth revision*).

†Rules for rounding off numerical values (*revised*).

#### 1. SCOPE

**1.1** This standard covers the requirements and tests for axial flow fans having impellers directly coupled to the shaft of electric motors or indirectly driven by electric motors. In the case of indirectly driven fans, the electric motor shall conform to the relevant Indian standard.

**1.2** The fans for use under free flow conditions are excluded from the scope of this standard.

**1.3** Axial flow fans for use in mines and hazardous atmospheres may require additional requirements to be met, not covered by this standard.

#### 2. TERMINOLOGY

**2.0** For the purpose of this standard, the following definitions, in addition to those given in IS : 1885 ( Part 55 )-1981\* shall apply.

**2.1 Axial Flow Fan** — A fan having a cylindrical casing in which the air enters and leaves the impeller in a direction substantially parallel to its axis.

**2.2 Fan** — A rotary machine which maintains a continuous flow of air at a pressure ratio not normally exceeding 1.3.

**2.3 Air** — The term air has been used as an abbreviation for 'air or any other gas' except where referred to as 'atmospheric air'.

**2.4 Standard Air** — Atmospheric air having a specific weight of 1.2 kg/m<sup>3</sup> which is dry air at 20°C and 50 percent relative humidity with a barometric pressure of 760 mm Hg.

**2.5 Multi-Stage Fan** — A fan having two or more impellers working in series.

**2.6 Inlet Volume** — The volume per unit time entering the fan (  $Q_v$  ) expressed in m<sup>3</sup>/h.

**2.7 Air Power ( Total )** — That part of the energy, per unit time, imparted by the fan to the air in increasing its total pressure from that at the inlet to that at the outlet.

**2.8 Air Power ( Static )** — This is equal to the air power ( total ) less the nominal kinetic energy per unit time at the outlet.

\*Electrotechnical vocabulary : Part 55 Electric fans.

**2.9 Impeller Power** — The energy input per unit time to the fan impeller.

**2.10 Shaft Power** — The energy input per unit time to the fan shaft including the power absorbed by such parts of the transmission system as constitute an integral part of the fan, for example, fan shaft bearings.

**2.11 Fan Duty ( Total )** — The inlet volume dealt with by the fan at the stated fan total pressure.

**2.12 Fan Duty ( Static )** — The inlet volume dealt with by the fan at a stated fan static pressure.

**2.13 Net Fan Total Efficiency** — The ratio of the air power ( total ) to the impeller power.

**2.14 Net Fan Static Efficiency** — The ratio of the air power ( static ) to the impeller power.

**2.15 Fan Total Efficiency** — The ratio of the air power ( total ) to the shaft power.

**2.16 Fan Static Efficiency** — The ratio of the air power ( static ) to the shaft power.

**2.17 Side Tube or Static Pressure Tube** — A tube which allows air to flow without disturbance, past one or more small orifices having their axis at right angles to the direction of air stream in which it is placed.

**2.18 Side Tapping or Static Pressure Tapping** — A small opening in the wall of an airway, having its axis at right angles to the wall and so constructed as to allow the air to flow past without disturbance.

**2.19 Facing Tube or Total Pressure Tube** — An open ended tube, the axis of which is coincident with the direction of the air stream in which it is placed, the open end facing upstream, that is, against the direction of flow.

**2.20 Pitot Tube** — A combination of side tube and facing tube as one unit.

**2.21 Cooling Air Temperature** — The temperature of the surrounding atmosphere in which the fan operates.

**2.22 Type Tests** — Tests carried out to prove conformity with the requirements of this standard. These are intended to prove general qualities and design of a given type of fan.

**2.23 Routine Tests** — Tests carried out on each fan to check the essential requirements which are likely to vary during production.

**2.24 Acceptance Tests** — Tests carried out on samples selected from a lot for the purpose of verifying the acceptability of the lot.

### 3. SIZES

**3.1** The following shall be the preferred sizes:  
300, 375, 475, 600, 750, 900, 1 200 and 1 500 mm.

NOTE — Other sizes are also permitted subject to agreement between the purchaser and the supplier.

### 4. RATED VOLTAGE

**4.1** The preferred rated voltages for axial flow fans shall be 230, 240 V, single-phase and 400, 415 V, three-phase ( *see* IS : 585-1962\* ).

### 5. FREQUENCY

**5.1** The rated frequency shall be the standard frequency of 50 Hz.

NOTE — Nevertheless, fans made for other frequencies shall be considered to comply with these specifications provided they do so in all other relevant respects.

### 6. DESIGN AND GENERAL CONSTRUCTION

**6.1 Motor Enclosure** — The enclosure of the fan motor shall be of the totally enclosed type.

**6.2 Rotor** — The rotor of the fan motor shall be well-balanced.

**6.3 Blades** — Fans shall be fitted with two or more well-balanced blades made from metal or other suitable material. The blades and blade carriers shall be securely fixed so that they do not loosen in operation.

**6.4 Mounting** — The means provided for securing the fan mounting or fan casing shall be such as to provide a secure fixing. Where the casing contains members to be clamped against an exterior wall, these shall be capable of being sealed to prevent the ingress of rain-water at the point of attachment.

**6.5 Guards** — Suitably designed guards shall be made available by the manufacturer and supplied on request, and shall be fitted either to the inlet or the outlet side, or both, to prevent accidental contact with the rotating blades. The guards shall be securely attached and shall be adequately rigid to resist accidental contact with the blades. When the guards are in two pieces, positive locking arrangement to keep the two pieces together should be made.

**6.6 Bearings** — If necessary, the manufacturer shall, on inquiry, furnish information about the type of bearings and instructions for their proper lubrication ( *see* Appendix A ).

\*Voltages and frequency for ac transmission and distribution systems ( *revised* ).

**6.7 Protective Measures** — An earthing terminal of adequate current-carrying capacity conveniently located and easily accessible shall be provided. In the case of fans for use on three-phase, two separate earthing terminals shall be provided.

## 7. GENERAL AND SAFETY REQUIREMENTS

**7.1 Protection Against Electric Shock** — In the assembled fan, live parts shall not be accessible to the standard test finger (see IS : 1401-1970\*). This requirement is applicable for all positions in the normal use.

**7.2 Electric Insulation** — When measured according to the method specified in 10.5, the insulation resistance shall be not less than 2 MΩ.

**7.2.1 Leakage Current** — Requirements of relevant Indian standards on motors shall apply. The leakage current which may flow from the live parts to the accessible parts and metal foil on external insulating material connected together shall not exceed 300 μA (peak), that is 210 μA (rms).

**7.2.2** There shall be no breakdown of the insulation when the fan is subjected to high voltage test as given in 10.3 or flash test (10.4), as the case may be.

**7.3 Insulating Materials** — Windings of fans and regulators (where provided) shall be insulated with either Class A, Class E or Class B insulating materials which comply with the limits of temperature-rise specified in 7.4. These insulating materials are detailed in IS : 1271-1985†.

**7.4 Temperature-Rise** — The fan motor shall be tested at any cooling air temperature not exceeding 40°C, but whatever may be the value of this temperature, the permissible temperature-rise when measured as described in 10.14.2 shall not exceed the limits given in Table 1.

\*Specification for accessibility test probes (first revision).

†Thermal evaluation and classification of electrical insulation (first revision).

**7.5 Finish** — All the surfaces of the assembly and mechanism of both fan and regulator, if any, shall be of corrosion resisting material or shall be suitably and durably protected against corrosion.

## 7.6 Speed Regulators

**7.6.1** It is not usual for fans covered by this specification to be provided with regulators. However, if regulators are required, this shall be a matter of agreement between the purchaser and the supplier.

**7.6.2 Enclosure** — Enclosures of the fan regulators shall either be of the ventilated type or the totally-enclosed type.

**7.6.3** Where a regulator is provided with a capacitor not permanently connected across the motor terminals, provision shall be made for the capacitor to be discharged when the regulator is in the 'off' position.

**7.6.4** The regulator handle or knob shall either be of insulating material or of metal. If of metal, it shall be adequately insulated electrically and thermally. All metallic parts associated with it shall be protected from accidental contact.

**7.6.5** The regulator handle or knob shall be so placed that it can be safely and conveniently manipulated with definite positioning action. The handle or knob shall be so designed that it does not become loose in use. The 'Running' and 'Off' positions of the regulator shall be distinctly and clearly marked and the indicator on the operating handle or knob shall correctly indicate the position of the regulator.

**7.6.6** The mechanism of the regulator shall be so designed as to ensure positive contact at each running position. In the case of induction type regulator, it is essential that no portion of the induction winding remains permanently short-circuited in any of the running positions.

**7.6.7** The regulators shall have mechanical stops for the regulator moving contact to prevent accidental contact with the metallic body of the regulator in the event of forced overtravel of the knob.

TABLE 1 PERMISSIBLE LIMITS OF TEMPERATURE-RISE

(Clauses 7.4, 10.14.2 and 10.14.2.1)

Sl. No.	PART OF MOTOR OR REGULATOR	TEMPERATURE-RISE, °C			METHOD OF MEASUREMENT
		Class A Insulation	Class E Insulation	Class B Insulation	
(1)	(2)	(3)	(4)	(5)	(6)
i)	Insulated windings of motors	60	75	80	Change of resistance
ii)	Insulated windings, if any, of regulator (with continuous running on any contact)	60	75	80	Change of resistance
iii)	Regulator resistance unit (with continuous running on any contact)	The temperature-rise shall not reach such a value that there is a risk of injury to any insulating material on adjacent parts of the regulator			Thermometer
iv)	External surface likely to be touched during normal usage	40	40	40	Thermometer

7.7 Starters, if provided, shall conform to the requirements of the relevant Indian standards.

7.8 Silent Operation — Precautions shall be taken in the manufacture of fans and regulators to ensure a reasonable degree of silence at all speeds.

NOTE 1 — The need for specifying limits of noise levels ( acoustical ) of the fans is recognized. However, it has not been found possible to specify these limits at present on account of:

- a) dependency of these limits on the actual location of the fans,
- b) lack of data on the acceptable noise levels for different applications, and
- c) lack of agreed definition of noise level and method of evaluating the same.

The criterion of noise level may, therefore, be subject to an agreement between the manufacturer and the purchaser.

NOTE 2 — The values of noise level ( acoustical ) are under consideration.

8. PERFORMANCE REQUIREMENTS

8.1 Air Delivery Test — This test shall be carried out and computations made in accordance with 10.13.

8.2 Fan Characteristics — Fan characteristics curves shall be drawn after testing, considering not less than three test points determining a short part of the fan characteristic at different inlet volume flows and corresponding fan total or static pressure.

A system resistance line shall also be drawn, passing through the specified duty point such that

the total or static pressure varies as the square of the inlet volume flow ( see Fig. 1 ).

The most probable operating point for the fan shall be at the intersection of the fan characteristic and the system resistance line. The difference between the inlet volume flow at the intersection and the specified inlet volume flow ( that is the duty point ) shall be recorded as the measure of departure of the fan from the specified performance. This value shall fall within the range of specified tolerances.

The fan characteristic may be extended to zero inlet volume and to zero static pressure conditions but the portion of the characteristic which is beyond the range specified by the supplier shall not be taken into account for the purpose of performance detailed in Appendix B.

8.3 Tolerances on Ratings — The observed results expressed as percentage of the ratings assigned by the manufacturer shall be within the following limits:

Characteristic	Tolerance
Volume flow	− 5 percent
Static or total efficiency expressed as a percentage	− 5
Total power input	+ 10 percent
Speed	± 10 percent

Where a tolerance in one direction is omitted, there is no restriction on the value in that direction.

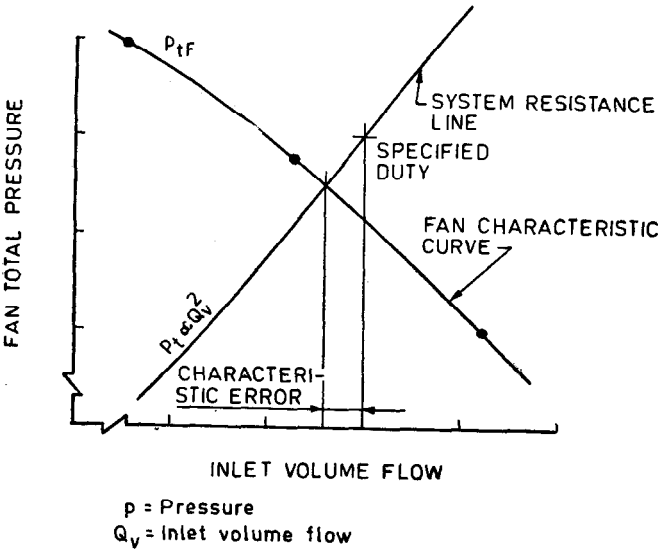


FIG. 1 EXAMPLE OF FAN CHARACTERISTIC CURVE AND TEST FOR A SPECIFIED DUTY



## 9. MARKING

**9.1** Each fan shall be indelibly marked with at least the following information:

- a) Manufacturer's name, trade-name of fan, if any, and serial number;
- b) Rated voltage(s) or voltage range and number of phases;
- c) Input in watts;
- d) Size of fan;
- e) Rated speed of fan in rev/min;
- f) Frequency of power supply;
- g) Direction of rotation and direction of air flow (marking should be of permanent nature);
- h) Air delivery at test voltage and stated duty; and
- j) Country of manufacture.

**9.1.1** Fans shall be marked in a legible and indelible manner on or adjacent to these terminals with the symbol  $\perp$ .

**9.2** For additional information that the manufacturer may be requested to supply, see Appendix A.

**9.3** For additional information that the purchaser may be requested to supply, see Appendix C.

**9.4** Axial flow fans may also be marked with the Standard Mark:

**NOTE** — The use of the Standard Mark is governed by the provisions of the Bureau of Indian Standards Act 1986 and the Rules and Regulations made thereunder. The Standard Mark on products covered by an Indian Standard conveys the assurance that they have been produced to comply with the requirements of that standard under a well defined system of inspection, testing and quality control which is devised and supervised by BIS and operated by the producer. Standard marked products are also continuously checked by BIS for conformity to that standard as a further safeguard. Details of conditions under which a licence for the use of the Standard Mark may be granted to manufacturers or producers may be obtained from the Bureau of Indian Standards.

## 10. TESTS

### 10.1 Categories of Tests

**10.1.1 Type Tests** — The tests specified below shall constitute type tests and shall be carried out on three samples of same type and rating selected, preferably, at random from a regular production lot:

- a) High voltage ( 10.3 ),
- b) Insulation resistance ( 10.5 ),
- c) Earthing continuity ( 10.6 ),
- d) Electrical input ( 10.7 ),
- e) Fan speed ( 10.8 ),
- f) Power factor ( 10.9 ),

- g) Starting ( 10.10 ),
- h) Moisture proofness ( for regulators only ) ( 10.11 ),
- j) Mechanical endurance ( for regulators only ) ( 10.12 ),
- k) Air delivery ( 10.13 ), and
- m) Temperature rise ( 10.14 ).

**10.1.2 Acceptance Tests** — The following shall constitute the acceptance tests:

- a) High voltage ( 10.3 ),
- b) Insulation resistance ( 10.5 ),
- c) Earthing continuity ( 10.6 ),
- d) Electrical input ( 10.7 ), and
- e) Fan speed ( 10.8 ).

**10.1.2.1 Sampling Plan** for acceptance tests is given in Appendix D.

**10.1.3 Routine Tests** — The following shall constitute routine tests:

- a) Flash test ( 10.4 ),
- b) Insulation resistance ( 10.5 ), and
- c) A simple running test to determine that the fan mechanism is in working order.

### 10.2 General Conditions of Test

**10.2.1 Test Voltage and Frequency** — Unless otherwise specified, the tests shall be carried out at rated voltage and frequency.

**10.2.1.1** When a rated voltage is indicated on the name plate, the tests shall be conducted at the rated voltage. If the fan is specified for two or more distinct rated voltages with three or more supply terminals, the tests shall be carried out at the most unfavourable voltage. In case of doubt, the tests shall be carried out at all voltages.

**10.2.1.2** When a rated voltage range is indicated on the name plate, the test shall be conducted at the mean of the upper and lower limits of the range provided that the upper limit does not exceed the lower limit by more than 10 percent.

If the upper limit exceeds this value, the test shall be conducted at the voltage corresponding to either the upper limit or the lower limit whichever is more unfavourable to the particular test.

**10.2.1.3 Limits of voltage variation** — The variation in the test voltage shall not exceed  $\pm 2$  percent of the test voltage during air delivery tests. While taking the current and watt readings during these tests, however, the voltage shall be maintained at the test voltage.

**10.2.2** For a fan rated with a range of frequency, the test shall be made at the frequency which gives the most unfavourable results. Tolerance on frequency shall be  $\pm 1$  percent.

**10.2.3 Limits of Error of Electrical Instruments —** The ammeters, voltmeters and wattmeters used for type tests shall have a Class index 0.5 or better [ see IS : 1248 ( Part 1 )-1983\* ]. For routine and acceptance tests, instruments of Class index 2 may be used.

### 10.3 High Voltage Test

**10.3.1** The source of supply for high voltage test shall be not less than 500 VA.

**10.3.2** The high voltage test shall be applied to all new and completed fan motors in normal working conditions with all parts in place except the capacitors which should be disconnected. As type test, this test should preferably be done immediately after the temperature-rise test.

**10.3.3** An ac test voltage at any convenient frequency between 40 to 60 Hz of approximately sine wave-form shall be applied and maintained for one minute without showing any kind of breakdown or flashover. The voltage should be applied starting with one-third of the full value, gradually increasing it to the full value which should be maintained for specified period after which the voltage should be gradually reduced.

The test voltage shall be applied as follows:

a) *For fan motors:*

- |  |             |
|--|-------------|
| i) Between line parts and body in the case of motors intended to be earthed  | 1 500 volts |
| ii) Between live parts and other inaccessible metal parts ( that is, over the functional insulation ) in the case of double insulated motors | 1 500 volts |
| iii) Between the inaccessible metal parts and the body ( that is, over the supplementary insulation ) in the case of double insulated motors | 2 500 volts |
| iv) Between live parts and body ( that is, over the reinforced insulation ) for reinforced insulated motor                                   | 4 000 volts |

b) *For regulators:*

- |  |             |
|--|-------------|
| i) Between any terminal and the body                               | 1 500 volts |
| ii) Between the terminals with the regulator in the 'OFF' position | 1 500 volts |

**10.3.4** At the end of one minute, the test voltage shall be removed and the insulation-resistance test conducted as in 10.5.

\*Specification for direct acting indicating analogue electrical measuring instruments and their accessories: Part 1 General requirements ( second revision ).

**10.3.5** If this test is required to be repeated, the test voltage levels shall be reduced to 85 percent of the original value.

### 10.4 Flash Test

**10.4.1** Every fan and regulator ( if provided ) shall withstand the voltage 20 percent higher than that specified in 10.3 for one second when it is applied instantaneously.

**10.4.2** Any other test similar to the one specified in 10.4.1 may be carried out as a routine test provided it will ensure the fan passing the high voltage test covered by 10.3.

### 10.5 Insulation Resistance Test

**10.5.1** Insulation resistance test shall be carried out on fans and regulators immediately after conducting the high voltage or flash test, as the case may be.

**10.5.2** The insulation resistance shall be not less than 2 megohms when tested with a dc voltage approximately 500 V applied between the points used for high voltage test or flash test.

**10.6 Earthing Continuity Test —** For fans intended to be earthed, the resistance shall not exceed 0.1 ohm between any exposed metal parts except the rotating parts supported by metal bearings, and

- the free end of the earthing conductor if the fan is fitted with a flexible cord, due allowance being made for the resistance of the earthing conductor of the flexible cord, or
- the earthing terminal or contact, when the fan is supplied without a flexible cord.

The resistance measurement shall be made with a current of 10 A with a dc voltage not exceeding 6V.

**10.7 Electrical Input Test —** The electrical input to the fan in watts shall be determined by running the fan at the test voltage and at the highest speed.

**10.8 Fan Speed Test —** The speed of rotation of the fan shall be determined by running the fan at the test voltage and its rated frequency. The method of measurement of the speed of fan shall be such that the speed of the fan is not appreciably affected.

**10.9 Power Factor Test —** The power factor of the fan when tested at the test voltage and the highest speed of the fan shall not be less than:

- 0.90 for capacitor type fans, and
- 0.60 for non-capacitor type fans.

**10.10 Starting —** The fan shall be capable of starting up from rest at the lowest speed step when 85 percent of the rated voltage or 85 percent of the lowest voltage in the voltage range is applied.

**10.11 Moisture Proofness ( for Regulators only )** — The regulator shall be subjected to and shall satisfy the high voltage and insulation resistance tests immediately after having been placed for a period of 24 hours without the current being passed through the regulator in a closed receptacle in which relative humidity is maintained between 90 to 95 percent at any temperature chosen in the range of 40 to 50°C. Whatever temperature is chosen for this test, it shall be maintained constant to within  $\pm 1^\circ\text{C}$ .

**10.12 Mechanical Endurance Tests ( for Regulators only )** — The regulator shall continue to function satisfactorily after being subjected to a test of 1 500 operations when connected to a fan with full load current flowing through the fan or an electrical load of an equivalent impedance supplied at the maximum rated voltage. One operation includes a full cycle of movement from the 'OFF' position to the 'Full Speed' position ( or to the other extreme position ) and back to 'OFF'. The test shall be made at the rate of approximately 6 operations per minute.

**10.13 Air Delivery Test** — This test shall be carried out with the guard, if any, in position.

**10.13.1** To the fan inlets shall be attached a straight cylindrical airway of diameter  $D$  and minimum length  $4D$ ;  $D$  may differ from the fan inlet diameter by not more than 20 percent larger or 5 percent smaller; a conical expander or reducer of  $15^\circ$  maximum included angle being used to connect the fan to the airway.

**10.13.2** If the fan is fitted with an inlet flare, the outside diameter of the flare may be regarded as the fan inlet for connection to the test duct. If more convenient, the flare may be removed for the test.

**10.13.3** The fitting of any additions to the fan for the purpose of this test shall be subjected to the following provisions:

- No additions or alterations solely for the purpose of a test shall be made to the fan as supplied except that when an addition to the fan that may affect its performance has been specified, and unless otherwise agreed to between the manufacturer and the purchaser, the addition shall be fitted for the test. Such an addition shall then be regarded as a part of the fan.
- An allowance shall be made for losses due to the friction of air in the airway between the fan and the point at which the readings are taken according to formula (5) given in 10.13.10.
- In any test, the airways shall be made reasonably airtight. When provision is made for insertion and manipulation by measuring instruments, care shall be taken to eliminate leakage as far as possible.
- Care should also be taken to avoid any obstructions which may modify the air flow, either at the inlet or at the outlet of the airways.

**10.13.4** The inlet end of the test airway shall be fitted with a conical inlet and four side tappings in accordance with Fig. 2 and with the following provisions:

- The proportions and tolerances of the conical inlet are given in Fig. 2 together with relevant notes on manufacture and installation. The inlet airway diameter  $D$  used in the computation shall be measured after manufacture.

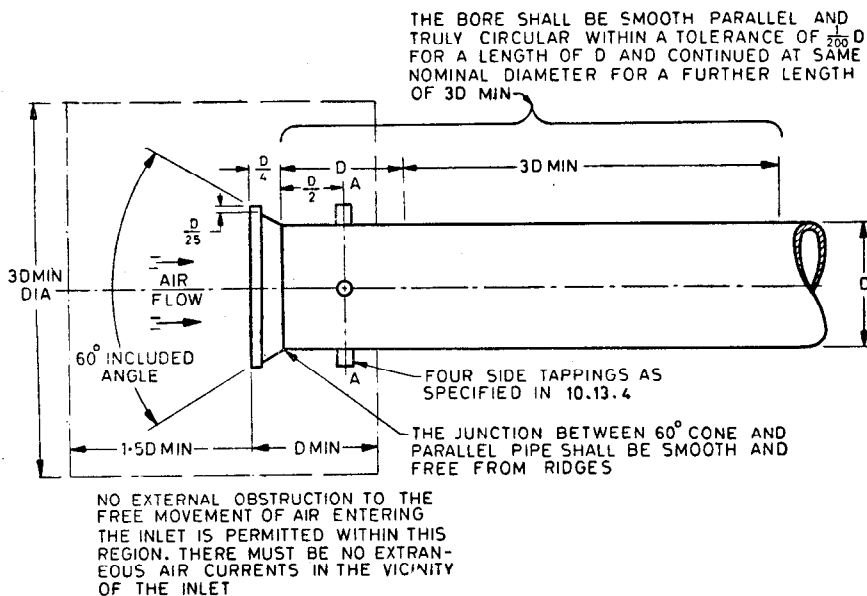


FIG. 2 CONICAL INLET

- b) The four side tappings at plane *AA* shall be equally spaced at  $90^\circ$  on the cylindrical duct. The bore at the surface of the airway shall not exceed 4.76 mm in diameter and shall be straight, uniform and at right angles to the duct for at least 2 bore diameters. The openings shall be flush with the duct and free from burrs and countersinks. The four side tappings shall be connected to one limb of the manometer, each connection being of the same length, bore and arrangement of tubing to minimize the effect of flow due to difference of pressure at the tappings. The other limbs of the manometer shall be opened to the ambient atmosphere and the manometer reading shall be taken as equal to the average static pressure in the airway.
- c) *Coefficient of discharge* — The coefficient of discharge of the conical inlet installed as above is given in Table 2. For Reynolds numbers of 400 000 and above, the coefficient of discharge is 0.975 and will cover the majority of fan tests. When the air flow in cubic metres per hour, numerically, is less than 16 700 times the airway diameter in meters, then the coefficient of discharge shall be taken appropriate to the Reynolds number given in Table 2.

**TABLE 2 DISCHARGE COEFFICIENTS FOR REYNOLDS NUMBER ( $Re$ )**

REYNOLDS NUMBER ( $Re$ )	20 000*	40 000	60 000	100 000	200 000	300 000	400 000	and above
DISCHARGE COEFFICIENT, $C_D$	0.930	0.940	0.945	0.953	0.967	0.973	0.975	

\*A conical inlet shall not be used at Reynolds number less than 20 000.

Intermediate values of  $C_D$  may be obtained by linear interpolation.

The Reynolds number for standard air is given by  $Re = \frac{23.58 Q}{D}$  using the notation of 10.13.10

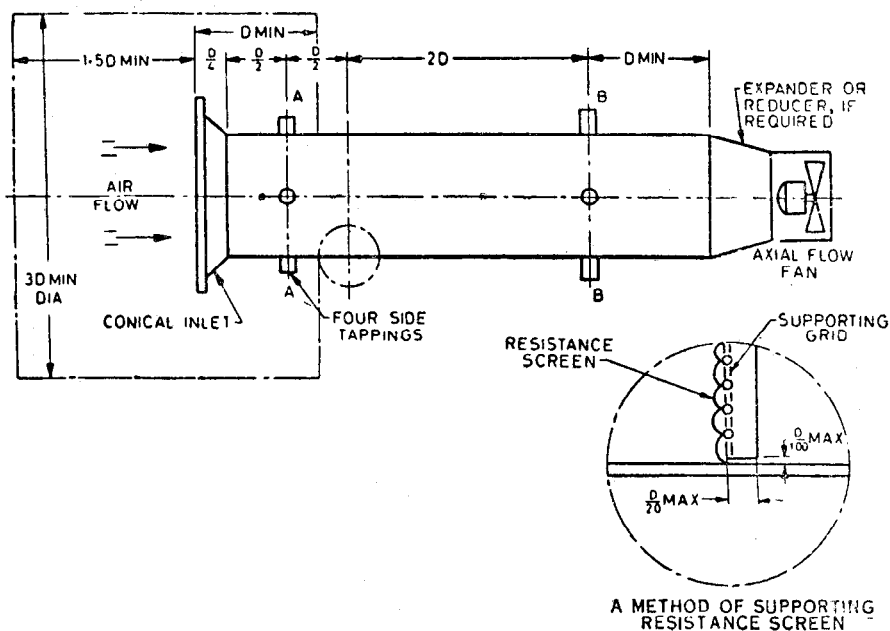
and this may be taken to determine the coefficient of discharge with negligible error for all normal variations in ambient conditions.

**10.13.5** A resistance comprising a screen having evenly spaced aperture of uniform size, not exceeding  $D/20$  should be fitted at a distance  $D$  from the commencement of the cylindrical portion of the inlet. The screen may be composed of one or more layers of even wire or fabric supported by a wire guard.

**10.13.6** The static pressure data can be obtained by changing the screen or adding additional screens in the test duct. If a ring is secured inside the test airway to support the screen, or when a ring is used to stiffen the periphery of the fabric or the other screen, the radial thickness of the ring shall not be greater than  $D/100$  (see Fig. 3).

**10.13.7** At plane *BB*, distant  $2D$  downstream from the resistance screen, there shall be four side tappings, similar to those in plane *AA*, and connected to the low pressure limb of a monometer, the other limb being connected to the ambient pressure in the vicinity of the fan discharge.

**10.13.8** The volume per unit time at plane *AA* shall be computed by using formula (1) and corrected to fan inlet conditions for any change in the air density between plane *AA* and the fan inlet *BB*.



**FIG. 3 ARRANGEMENT FOR AIR DELIVERY TEST**

**10.13.9 Air temperatures in the inlet airway** shall be taken by providing a thermometer with its probe inside the air way near section *BB*. The inlet volume so compiled shall then be used to calculate the velocity pressure at plane *BB* using formulae (2) and (3). For the purpose of this test, the algebraic sum (with the sign reversed) of the static pressure at plane *BB*, and the velocity pressure at plane *BB*, plus a friction allowance for all test ducting downstream of plane *BB*, in accordance with formula (5) shall be taken as the fan total pressure.

**10.13.10 Formulae and Computation of Results** — The following formulae shall be used for the computation of results of the tests laid down in 10.13:

- a) Inlet volume per unit time

$$Q = 12\,500 \times C_D \times D^2 \sqrt{\frac{\Delta P}{W_t}} \text{ m}^3/\text{h} \quad \dots (1)$$

where

$C_D$  = coefficient of discharge,

$D$  = diameter of airway in metres,

$\Delta P$  = difference between ambient pressure in the vicinity of the inlet and the average pressure at the side tappings at plane *AA* in mm  $\text{H}_2\text{O}$ ; and

$W_t$  = weight of air in airway at the test temperature  $t^\circ\text{C}$ , in  $\text{kg}/\text{m}^3$ .

- b) Weight per unit volume of atmospheric air at test section

$$W_t = 1.205 \times \frac{B + 0.0737 P_s}{760} \times \frac{293}{(273 + t)} \text{ kg}/\text{m}^3$$

which may be very closely approximated as

$$W_t = 1.2 \times \frac{B + 0.0737 P_s}{760} \times \frac{293}{(273 + t)} \text{ kg}/\text{m}^3 \quad \dots (2)$$

[ taking  $1.205 \text{ kg}/\text{m}^3$  (approximated to  $1.2 \text{ kg}/\text{m}^3$ ) as the weight of standard air at  $20^\circ\text{C}$  and  $760 \text{ mm Hg}$  ].

where

$B$  = barometric pressure in mm Hg at the time of test, and

$P_s$  = static pressure in mm  $\text{H}_2\text{O}$ .

- c) Velocity of air at a point

$$V = 16\,000 \sqrt{\frac{P_v}{W_t}} \text{ m}/\text{h} \quad \dots (3)$$

- d) Average velocity of air in the airway

$$\bar{V} = \frac{Q}{A} \text{ m}/\text{h} \quad \dots (4)$$

where

$A$  is the area of airway in square metres.

- e) Friction loss in airway

$$P_f = 0.02 \frac{L}{D} \times P_v \text{ mmH}_2\text{O} \quad \dots (5)$$

where

$L$  and  $D$  = length and diameter of airway in metre, respectively; and

$P_v$  = velocity pressure in  $\text{mmH}_2\text{O}$ .

**10.13.11 Method of calculation of efficiency** is given in Appendix B.

## 10.14 Temperature-Rise Test

**10.14.1 Measurement of Cooling Air Temperature During Tests** — The cooling air temperature shall be measured by means of several thermometers placed at different points around the fan motor at a distance of 1 to 2 m and protected from all heat radiations and extraneous draughts. The thermometers used for this test shall be accurate to  $\pm 0.5^\circ\text{C}$ .

The value to be adopted for the temperature of the cooling air during a test shall be the mean of the readings of the thermometers taken at equal intervals of time during the last quarter of the duration of test.

**10.14.2 Measurement of Temperature-Rise** — The temperature-rise measurements shall be carried out by the method indicated in Table 1, immediately after the air delivery test or after the fan has been run long enough to ensure that the temperature-rise has reached a steady state, using the following procedure.

**10.14.2.1** All temperature-rises to be measured by thermometer method [ items (iii) and (iv) of Table 1 ] shall be taken at the hottest accessible surface of the part, as also on the parts which are likely to cause injury to any adjacent insulating material.

**10.14.2.2** The method of measurement of temperature-rise by change in resistances is given below:

The temperature-rise  $t_2 - t_1$  may be obtained from the ratio of the resistances by the formula:

$$\frac{t_2 + 235}{t_1 + 235} = \frac{R_2}{R_1} \quad (\text{for copper windings})$$

$$\text{or } \frac{t_2 + 225}{t_1 + 225} = \frac{R_2}{R_1} \quad (\text{for aluminium windings})$$

where

$R_2$  = resistance of the winding at temperature  $t_2$  ( $^\circ\text{C}$ ) at the end of the test, and

$R_1$  = initial resistance of the winding at temperature  $t_1$  ( $^\circ\text{C}$ ) (cold).

From the above, the hot temperature ( $t_2$ ) can be expressed as:

$$t_2 = \frac{R_2}{R_1} (t_1 + 235) - 235$$

for the copper windings.

**APPENDIX A**( *Clauses 6.6 and 9.2* )**ADDITIONAL INFORMATION TO BE SUPPLIED BY THE MANUFACTURER**

**A-1.** The following additional information in respect of an electric axial flow fan shall be supplied by the manufacturer on request:

- a) Power factor,
- b) Number of blades,
- c) Type of regulator and number of running positions,
- d) Class of insulation,
- e) Type of bearings,
- f) Instructions for lubrication of bearings,
- g) Condenser value ( in case of single-phase fans ), and
- h) Fan total efficiency.

**APPENDIX B**( *Clauses 8.2 and 10.13.11* )**METHOD OF CALCULATION OF EFFICIENCY**

**B-1.** The performance of the fan at a stipulated air delivery  $Q$  and fan total pressure  $P_t$  shall be expressed by the 'total efficiency'  $\eta_t$  which may be expressed as the ratio of air power ( total )  $P_{total}$  to the shaft power,  $P_{shaft}$ .

$$\text{Thus } \eta_t = \frac{P_{total}}{P_{shaft}} \quad \dots (6)$$

The air power ( total ) may be obtained from the formula:

$$P_{total} = 2.725 \times 10^{-3} \times Q \times P_t \times K_p \text{ watts} \quad \dots (7)$$

where

$Q$  is in  $m^3/h$ ,

$P_t$  is in  $mmH_2O$ , and

$K_p$  is the compressibility coefficient having a value of unity for fan static pressure not exceeding 255  $mmH_2O$  under normal atmospheric condition. At higher pressures  $K_p$  should be determined by reference to Fig. 3, calculating the pressure ratio by means of the formula given below:

$$K_p = \frac{\left( \frac{r-1}{p} \right)^r - 1}{(p-1)(r-1)} \quad \dots (8)$$

where

$r$  = ratio of specific heat at constant pressure to specific head at constant volume.

The value of  $r$  may be taken as 1.4 for atmospheric air  $P_{shaft}$ .

Pressure ratio ( $p$ ) ( for exhausting conditions which apply to test method described in 10.13 ) is given by

$$p = \frac{B}{B - 0.0737 P_s} \quad \dots (9)$$

using the notations of 10.13.10 (b).

The shaft power, shall be obtained, for the purpose of this specification from the following relation:

$$P_{shaft} = [ P_L - ( \text{fixed losses} + \text{copper losses} + \text{stray load losses} ) ]$$

where

$P_L$  = power input to the motor with the fan coupled to the motor and run at rated duty and speed in watts.

The fixed losses and copper losses shall be calculated in accordance with details given in IS : 4889-1968\*. The copper losses shall be calculated on the corresponding current at the duty point of the fan.

The stray load loss is assumed to be 0.5 per cent of the shaft power.

\*Methods of determination of efficiency of rotating electrical machines.

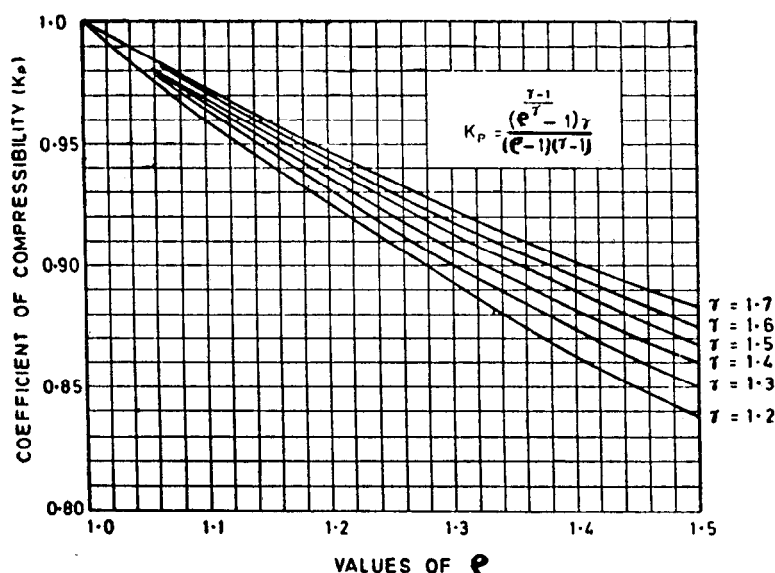


FIG. 4 GRAPH FOR DETERMINING THE COEFFICIENT OF COMPRESSIBILITY ( $K_p$ ) WHEN THE GUARANTEED FAN STATIC PRESSURE EXCEEDS 255 mm H<sub>2</sub>O UNDER NORMAL ATMOSPHERIC CONDITIONS

## APPENDIX C

( Clause 9.3 )

### INFORMATION TO BE SUPPLIED BY THE PURCHASER

**C-1.** The following information in respect of an electric axial flow fan shall be supplied by the purchaser on request:

- a) Size;
- b) Electric supply details;
- c) Air delivery at stated duty;
- d) Nature of medium, air or other gases;
- e) Atmospheric conditions; and
- f) Altitude of the place where the fan is to be installed.

## APPENDIX D

( Clause 10.1.2.1 )

### SAMPLING PLAN FOR ACCEPTANCE TESTS

#### D-1. LOT

**D-1.1** All the fans of the same size and rating manufactured from the same material under similar conditions of production in a factory shall be grouped together to constitute a lot.

#### D-2. SCALE OF SAMPLING

**D-2.1** For judging the conformity of the lot to the requirements of acceptance tests, sampling shall be done for each lot separately. For this purpose, the number of fans to be selected at random from each lot shall depend upon the size of the lot and shall be in accordance with col 1 and 2 of Table 3.

TABLE 3 SAMPLE SIZE AND ACCEPTANCE NUMBER

LOT SIZE	SAMPLE SIZE		ACCEPTANCE NUMBER	FIRST REJECTION NUMBER	SECOND REJECTION NUMBER
	First Sample	Second Sample			
(1)	(2)	(3)	(4)	(5)	(6)
Up to 25	3	3	0	2	2
26 „ 50	5	5	0	2	2
51 „ 100	8	8	0	2	2
101 „ 300	13	13	0	2	2
301 and above	20	20	0	3	4

**D-2.2** In order to ensure the randomness of selection, procedures given in IS : 4905-1968\* may be followed.

### **D-3. CRITERIA FOR CONFORMITY**

**D-3.1** The number of fans selected at random in accordance with col 1 and 2 of Table 3 shall be subjected to all the acceptance tests. A fan failing to meet any of the requirements of the acceptance tests shall be termed as defective. The lot shall be considered as conforming to the requirements

of acceptance tests if there is no defective in the sample and shall be rejected if the number of defectives in the sample is greater than or equal to the first rejection number given in col 5 of Table 3. If the number of defectives is between the acceptance number and the first rejection number, the second sample of the same size ( as given in col 3 ) shall be selected from the lot at random and subjected to the acceptance tests. If the total number of defectives in both the samples combined is less than the second rejection number given in col 6 of Table 3, the lot shall be accepted, otherwise not.

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\*Methods for random sampling.



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